Service.





The 2.0 I 110 kW engine with petrol direct injection (FSI)

Self Study Programme 279

Improved methods of injecting petrol into the intake port represent more or less the limit of what can be done to optimise economy with conventional techniques. The direct injection principle opens up new possible ways of creating more economical and environmentally sound petrol engines. Thrifty diesel engines employ direct injection, in other words, the amount of fuel supplied corresponds exactly to the requirements at any given time.



The logical next step - at least in theory - would therefore be to apply the principle of direct injection to petrol engines as well.

FSI technology from Audi opens up a whole new dimension for the petrol engine.

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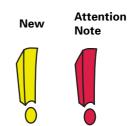
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The Self Study Programme contains information on design features and functions.

The Self Study Programme is not intended as a Workshop Manual. Values given are only intended to help explain the subject matter and relate to the software version applicable when the SSP was compiled.

Use should always be made of the latest technical publications when performing maintenance and repair work.



Introduction

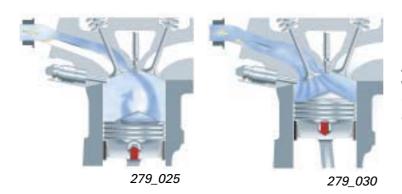


Highlights of the FSI engine

High-pressure injection system with newly developed single-plunger high-pressure pump

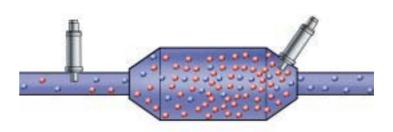


279_041



Air-controlled combustion process with map-controlled in-cylinder flow (stratified charge and homogeneous operation)

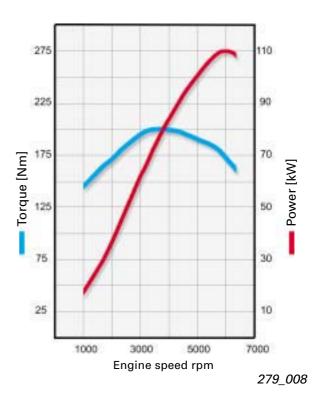
Enhanced exhaust gas treatment system with NO_x storage catalytic converter and NO_x sender



279_007

2.0 | FSI engine





Technical data:

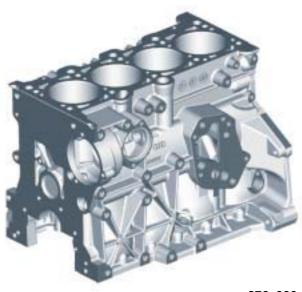
| Engine code letters: | AWA | | | | |
|------------------------------|---|--|-----|---|---|
| Capacity: | 1984 ccm | Valve timing: | | Inlet closes 48° after BI Exhaust opens 28° before Exhaust closes 8° before | |
| Bore: | 82.5 mm | | Exh | | |
| Stroke: | 92.8 mm | Inlet camshaft | | | |
| Compression ratio: | 11.5: 1 | | - | nge: 42° crankshaft | |
| Power: | 110 kW (150 hp) | Emission class | s: | EU IV | |
| Torque: | 200 Nm/ 3250-4250 rpm | Capacities: | | Engine oil incl. filter 4.8l | |
| Engine management system: | MED. 7.1.1 | Consumption: (5-speed manual gearb | | Urban Non-urbar Average | 9.9l/100 km 5.4l/100 km 7.1l/100 km |
| Valves: | 4 per cylinder | | | | |
| Valve timing: | Roller-type rocker fingers with hydraulic support elements | | | | |

Engine

Engine block

The engine block is made of an aluminium alloy and is the most compact type in its class with a cylinder spacing of 88 mm and an overall length of only 460 mm.

The engine block is identical to that of the 2.0 I engine with manifold injection (crankshaft, conrods, balance shafts and oil pump).



279_009

Crankcase breather

The blow-by gases are routed from the engine block directly into the first oil separator. The majority of the oil particles are removed from the gases in the oil separator labyrinth. From there, the gases pass via the hose connection into the integrated labyrinth of the cylinder head cover and then as virtually oil-free blow-by gases into the intake manifold by way of the pressure control valve.



279_046

Pistons

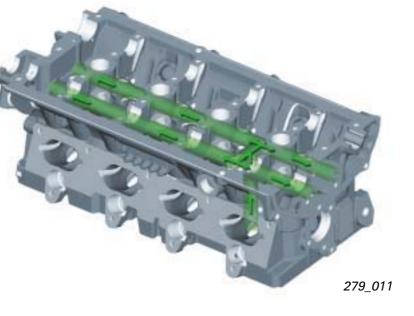
Use is made of lightweight aluminium alloy solid-skirt pistons with closely spaced piston pin bosses.

Advantage: Reduced oscillating masses and lower coefficients of friction as only a part of the piston skirt periphery runs in the cylinder.

A bowl incorporated into the piston crown aims the air flow directly towards the spark plug in stratified charge operation. The geometric shape of the piston causes the air flow to "tumble".

Oil circulation

The use of a 4-valve cylinder head with rollertype rocker fingers represents a major change in oil gallery design with respect to the 5-valve cylinder head with bucket tappets. Passing via the main oil gallery from the engine block, the oil enters the cylinder head between cylinders 3 and 4. Oil pressure is applied to the hydraulic support elements and camshaft bearings by way of two oil ducts. The support elements are provided with a spray orifice for lubrication of the roller-type rocker fingers. Further along the oil ducts, oil pressure is applied to the rotary motor for camshaft adjustment.









Engine

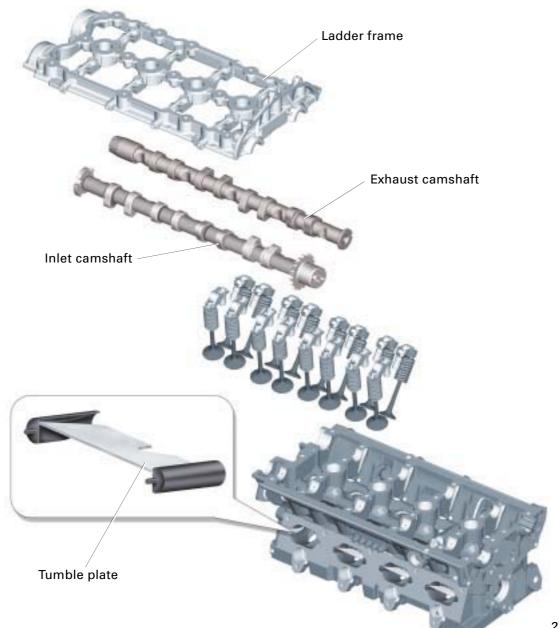
Cylinder head

The 4-valve cylinder head with roller-type rocker fingers is designed to suit the direct injection process.

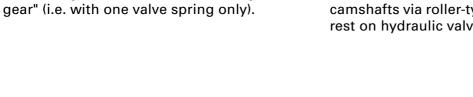
Valve timing is provided by way of two composite overhead camshafts rigidly mounted in a ladder frame.

The exhaust camshaft is driven by a toothed belt, which in turn drives the inlet camshaft by way of a simple chain. Each intake port is split into a top and bottom half by a tumble plate, the shape of which is designed to prevent incorrect installation.

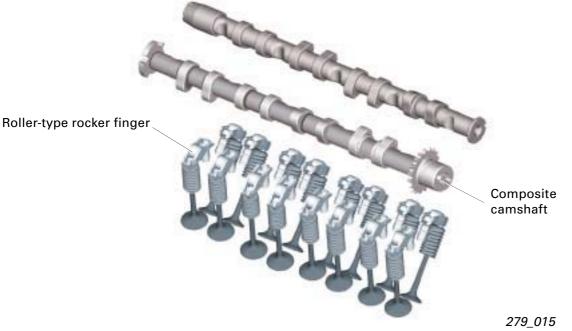
The mounts for the high-pressure injectors are integrated into the cylinder head, with the actual injectors projecting directly into the combustion chamber.



The valves are actuated by two composite camshafts via roller-type rocker fingers which rest on hydraulic valve lifters.



The valve gear takes the form of a "light valve



The valve cover is made of plastic and features a permanently attached elastomer seal.

The valve cover contains the pressure control valve for the crankcase breather and the internal oil separator.



Engine

Camshaft timing control

Continuous map-controlled hydraulic camshaft adjustment by up to 42° crank angle is achieved by way of a rotary motor.

The toothed belt drives the exhaust camshaft. The rotor of the motor is attached to the other end of the exhaust camshaft.

The stator is connected directly to the chain sprocket and drives the inlet camshaft via the chain.

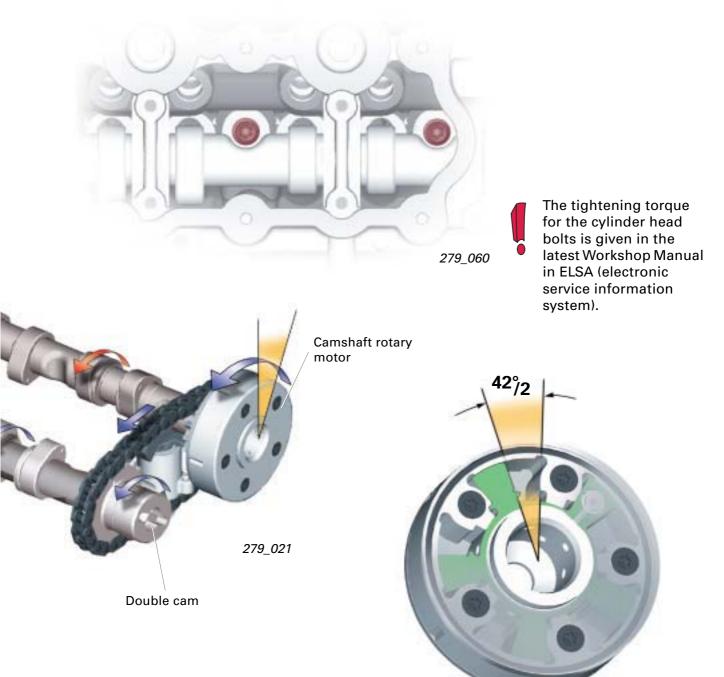
The stator adjustment is transmitted by way of the chain to the inlet camshaft, thus varying the inlet valve timing.

The Hall sender wheel and high-pressure pump drive are attached to the front and rear end of the inlet camshaft respectively.

> For details of camshaft timing control, refer to SSP 255

Camshaft positioning

The inlet and exhaust camshafts must be turned such that the recesses are vertically opposed. In this camshaft position the drive chain can be fitted without having to determine the number of rollers. This is also the only position in which the cylinder head bolts can be inserted and removed.



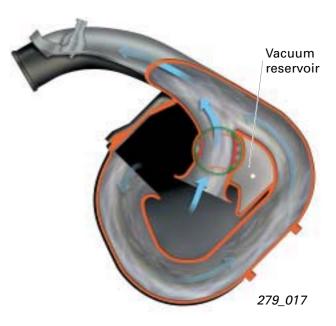


Engine

Intake manifold

The two-stage variable intake manifold promotes the desired power and torque characteristics. Pneumatic switching of the changeover barrel from torque to power position is map-controlled, with load, engine speed and temperature representing the relevant variables.

The vacuum reservoir is integrated into the intake manifold module.



Lower part of intake manifold

The lower part of the intake manifold contains four flaps which are driven by the intake-manifold flap motor -V157 via a joint shaft.

The potentiometer -G336 integrated into the motor provides the engine control unit -J220 with feedback on flap position.

The position of the intake-manifold flaps influences mixture formation and thus emission values. Intake-manifold flap control is classified as an emission-specific system and is monitored by the EOBD.

The lower part of the intake manifold is bolted to the fuel rail.



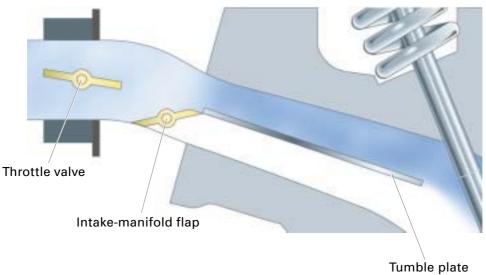
Intake air routing

There are two alternatives for air routing with the FSI system.

Version 1:

The intake-manifold flap is closed and the intake air mass thus routed over the tumble plate into the combustion chamber.

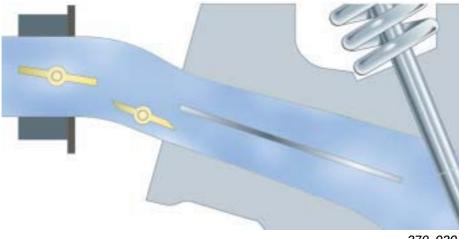
This method of air routing is used for stratified charge operation.



279_019

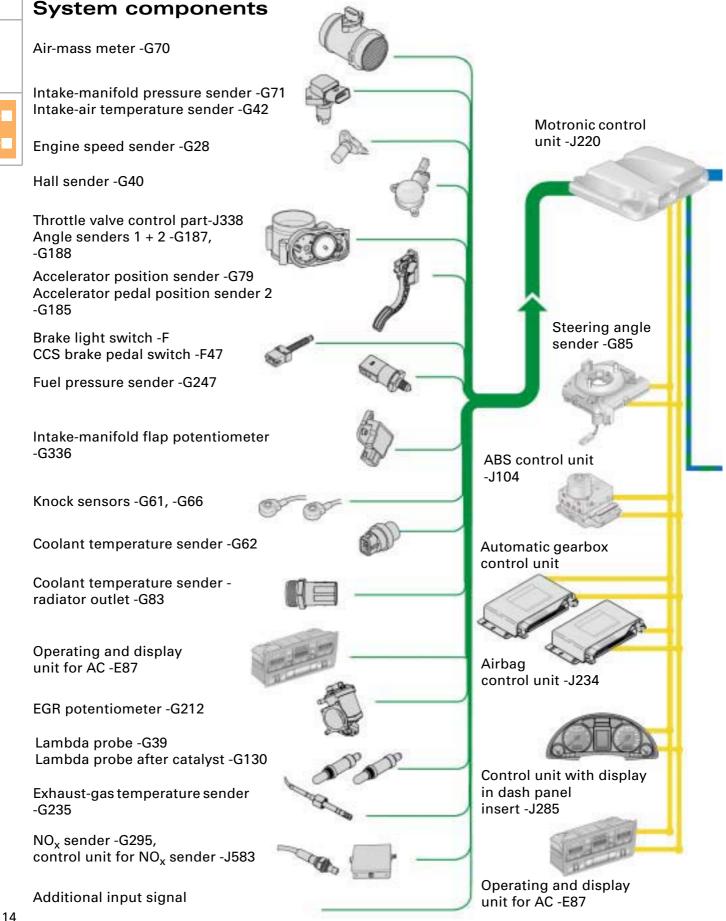
Version 2:

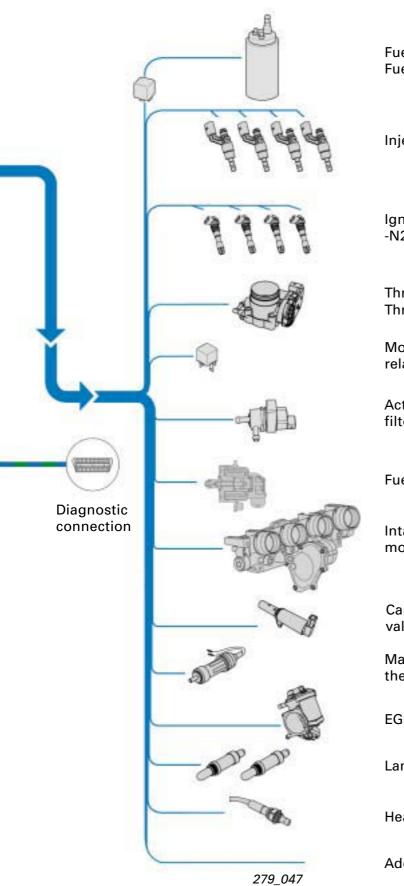
The intake-manifold flap is opened and the intake air mass thus routed over and under the tumble plate into the combustion chamber. This method of air routing permits homogeneous operation. Such a method is referred to as air-controlled combustion with map-controlled in-cylinder flow.



279_020

Engine management





Fuel pump relay -J17 Fuel pump -G6

Injectors, cylinders 1-4 -N30-33

Ignition coils 1-4 -N70, -N127, -N291, -N292

Throttle valve control part -J338 Throttle valve drive -G186

Motronic current supply relay -J271

Activated charcoal filter solenoid valve -N80

Fuel metering valve -N290

Intake-manifold flap motor -V157

Camshaft adjustment valve -N205

Map-controlled engine cooling thermostat -F265

EGR valve -N18

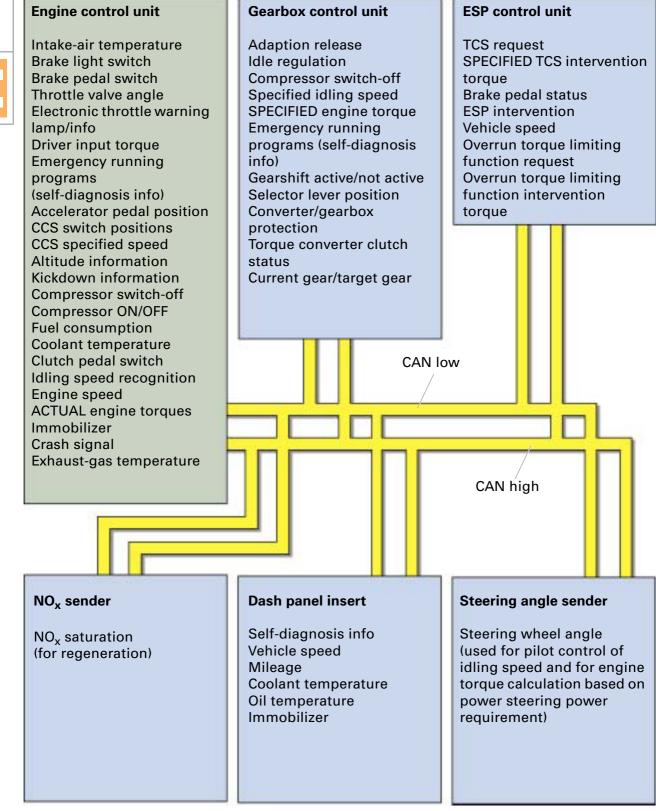
Lambda probe heaters -Z19, -Z29

Heater for NO_x sender -Z44

Additional output signals

Engine management

CAN bus interfaces



Engine control unit

Use is made for engine management of the Motronic control unit MED 7.1.1.

The designation MED 7.1.1 stands for:

- Μ = Motronic
- Е = Electronic throttle
- = Direct injection D
- 7. = Version
- 1.1 = Development status

The Bosch Motronic MED 7.1.1 incorporates petrol direct injection.

With this system the fuel is injected directly into the cylinder and not into the intake manifold.







Modes of operation

Whereas conventional petrol engines are reliant on a homogeneous air/fuel mixture, lean petrol direct injection engines can be operated with a high level of excess air in the part-throttle range by means of specific charge stratification.

There are two main modes of operation with the FSI system: Stratified charge operation in the part-throttle range and homogeneous operation in the full-throttle range.

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F les of operation are ind off the FSI concept. а T f operation are e reading measured С ction.

Engine management

Stratified charge operation

To achieve a stratified charge, injection, combustion chamber geometry and incylinder flow must be optimally matched in addition to satisfying certain prerequisites.



Namely:

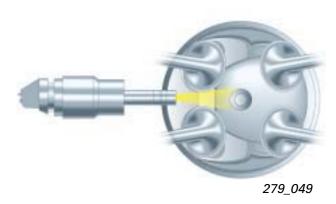
- Engine in corresponding load and engine-_ speed range
- No system faults of relevance to emissions
- Coolant temperature above 50 °C
- Temperature of NO_x storage catalytic converter between 250 °C and 500 °C

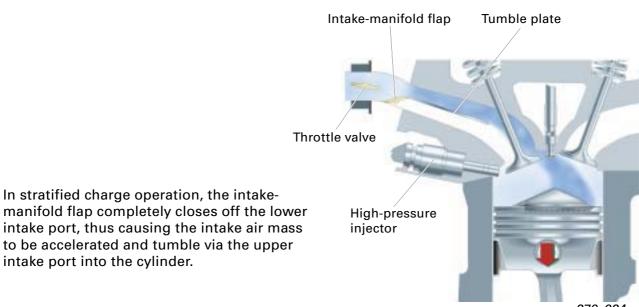
In stratified charge operation, the intake-

to be accelerated and tumble via the upper

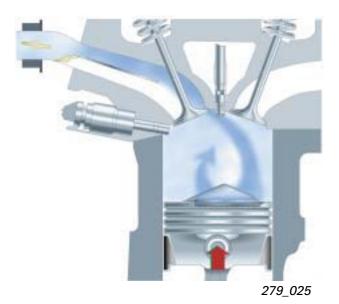
intake port into the cylinder.

- Intake-manifold flap closed





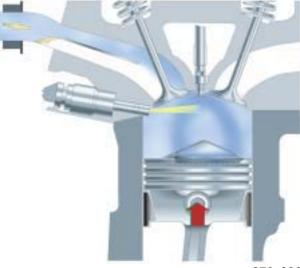
279_024



The tumble effect is further enhanced by the bowl in the piston. At the same time, the throttle valve is opened wide to minimise throttle losses.

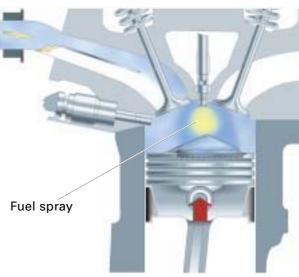
18

In the compression stroke, fuel is injected under high pressure (50-100 bar) into the area around the spark plugs just before the ignition point.

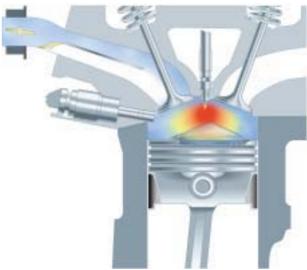




279_026



279_027



279_028

In view of the relatively shallow injection angle, the fuel spray scarcely comes into contact with the piston crown (so-called "aircontrolled" method).

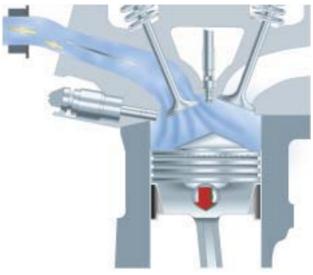
A mixture with good ignition properties forms around the spark plugs and is ignited in the compression phase. In addition, a layer of air forms between the ignited mixture and the cylinder wall after combustion, thus providing insulation and reducing heat dissipation via the engine block.

Engine management

Homogeneous operation

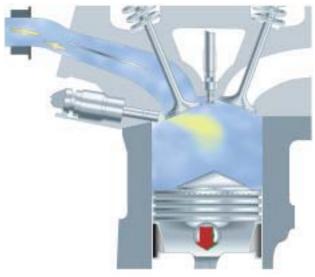


In the upper load and engine-speed range, the intake-manifold flap is opened to enable the intake air mass to flow into the cylinder via the upper and lower intake port.



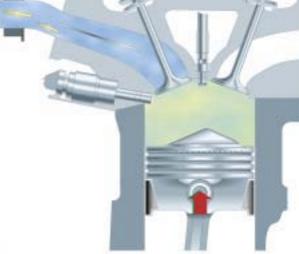
279_030

In contrast to stratified charge operation, fuel is not injected in the compression phase, but rather in the induction phase, producing a homogeneous charge (14.7:1) in the cylinder.



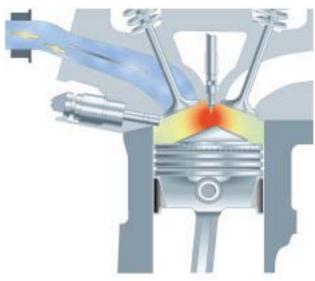
279_031

Injection in the induction stroke allows far more time to obtain an optimum air/fuel





279_032



279_033

The advantages of homogeneous operation are the result of direct injection in the induction stroke, in the course of which fuel vaporisation causes some of the heat to be extracted from the intake air mass. Such internal cooling reduces the knock tendency, which means the engine compression ratio can be increased and efficiency enhanced.

Combustion takes place in the entire combustion chamber without any insulating air and EGR masses.

mixture.

Engine management

Stratified charge operation is not possible over the entire map range. The range is restricted due to the fact that greater loads require a richer mixture and the fuel consumption advantage becomes progressively less. Combustion stability also deteriorates with Lambda values less than 1.4, as the mixture preparation time is no longer adequate with increasing engine speeds and the greater airflow turbulence has a negative effect.



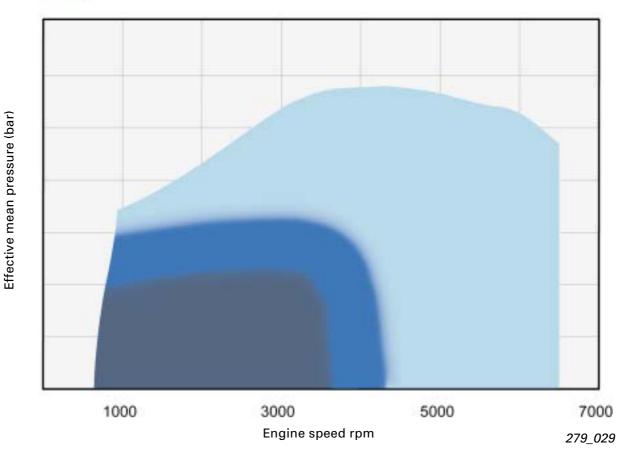
Homogeneous operation $\lambda = 1$ or $\lambda > I$ with 3-way catalytic converter

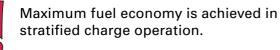


Homogeneous lean operation with $\lambda = 1.5$



Charge stratification with adapted in-cylinder flow and optimised EGR strategy





| | Self Study Programme Questionnaire |
|---|--|
| | What is your position within the Dealership? Please quote name, telephone number and fax number for reply and queries. |
| | Are the descriptions and explanations readily comprehensible? YES YES NO |
| A note to all users: | |
| This Self Study Programme is intended to familiarise readers with the 2.01110 kW engine with petrol direct injection (FSI). | YES A Page/Fig. No. |
| Your opinion matters to us. | |
| That is why we would like you to give us your thoughts on and any suggestions for future Self Study Programmes. The following questionnaire is designed to help you do so. | Is enough detail given on the subject matter relevant to your work? YES |
| Please make use of fax number 0049/841 89 36 36 7 for your suggestions. | |
| Thank you for your assistance. | Do you consider anything to have been overlooked? |
| Your Service Technology Training Team | NO |
| | Should further items he added to this guestion aris.2 |
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| | Remarks/miscellaneous: |
| | Please submit your questionnaire to the following fax number: |
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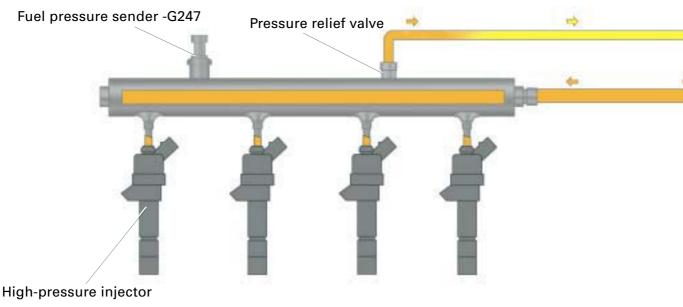
Engine sub-systems

Fuel system

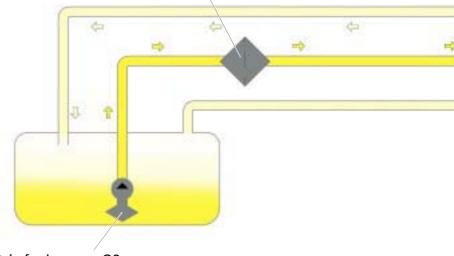
The fuel system consists of a low and high-pressure section.

In the low-pressure system, the fuel is conveyed by an electric fuel pump at approx. 6 bar via the filter to the high-pressure pump. The return flow from the high-pressure pump passes directly back to the tank.







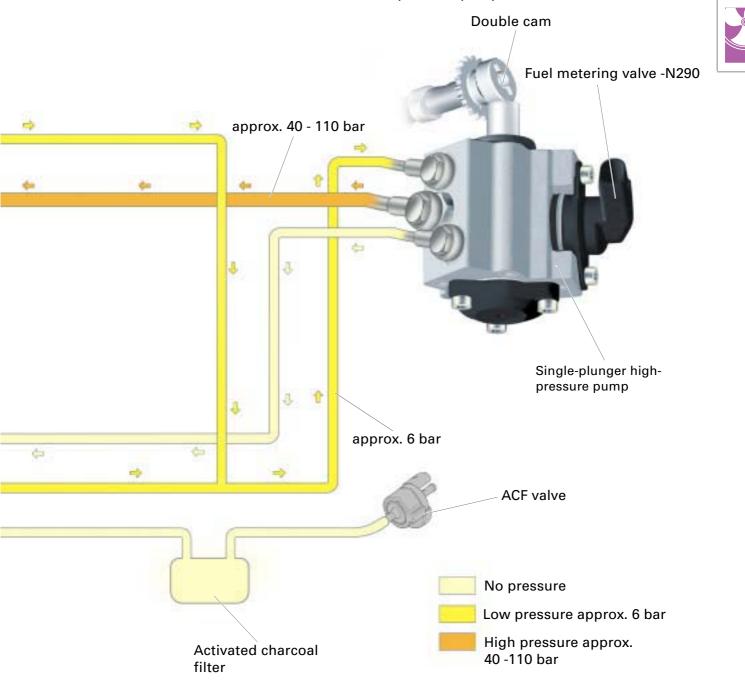


Electric fuel pump -G6

In the high-pressure system, the fuel flows at approx. 40 - 110 bar (depending on load and engine speed) out of the single-plunger high-pressure pump into the fuel rail, from where it is distributed to the four high-pressure injectors.

The pressure relief valve is designed to protect the components subjected to high pressure and opens as of a pressure of > 120 bar.

When the pressure relief valve opens, the fuel flows into the supply pipe to the highpressure pump.



279_034

Engine sub-systems

Single-plunger high-pressure pump

The single-plunger high-pressure pump with adjustable delivery rate is driven mechanically by the camshaft via a double cam.

The electric fuel pump provides the highpressure pump with a supply pressure of up to 6 bar.

The high-pressure pump generates the high pressure required in the rail.

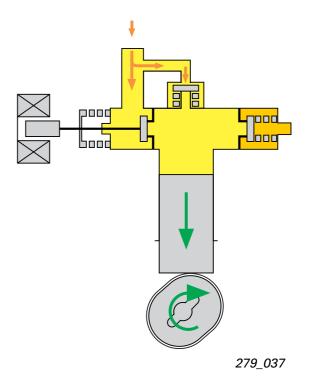


The pressure damper reduces fuel pressure pulsation in the system.



279 035

As the piston moves down, fuel flows at a supply pressure of approx. 6 bar from the intank pump via the inlet valve into the pump chamber.



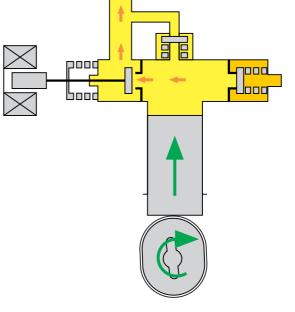
279_038

If the fuel metering valve opens prior to completion of the delivery stroke, the pressure in the pump chamber is dissipated and the fuel flows back into the fuel inlet. A non-return valve between pump chamber and fuel rail stops the rail pressure decreasing when the fuel metering valve opens.

As the piston moves up, the fuel is

compressed and conveyed into the fuel rail on exceeding the prevailing rail pressure. Located between pump chamber and fuel inlet is the switchable fuel metering valve.

To regulate the delivery rate, the fuel metering valve is closed as of pump cam BDC position until a certain stroke is reached. Once the necessary rail pressure has been attained, the fuel metering valve opens to prevent any further increase in pressure in the rail.



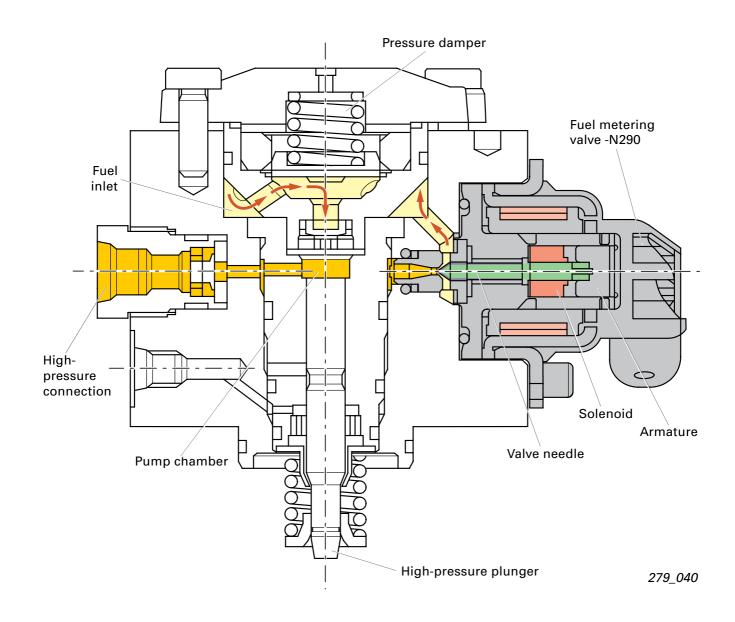
279_039

Engine sub-systems

Fuel metering valve -N290

For safety reasons, the fuel metering valve is designed as a solenoid valve which is open when deenergised.

Consequently, the entire delivery volume of the high-pressure pump is pumped back into the low-pressure circuit by way of the open valve seat. Energisation of the solenoid builds up a magnetic field which presses the valve needle connected to the armature into the valve seat. On attaining the rail pressure the fuel metering valve is no longer energised and the magnetic field collapses. The high pressure forces the needle out of the pump chamber and the fuel from the pump delivery chamber which is no longer required can flow back into the low-pressure circuit.

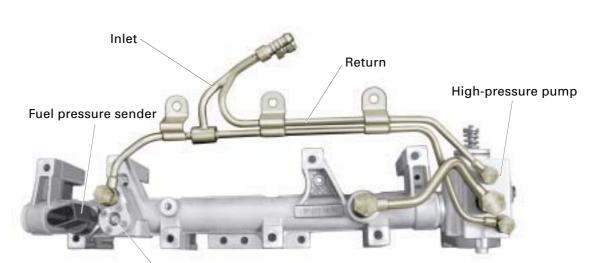




Fuel rail

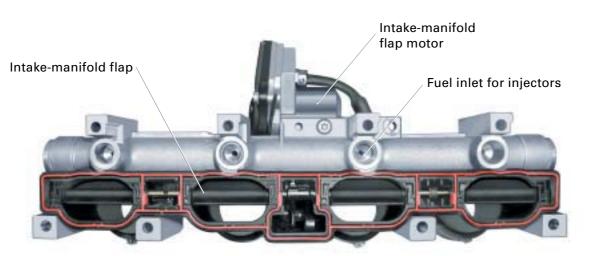
The rail is designed to distribute a defined fuel pressure to the high-pressure injectors and to provide an adequate volume for pressure pulsation compensation. It functions as a high-pressure accumulator and acts as a mount for injectors, fuel pressure sender, pressure limiting valve and high/low-pressure connections.





Pressure limiting valve

279_041





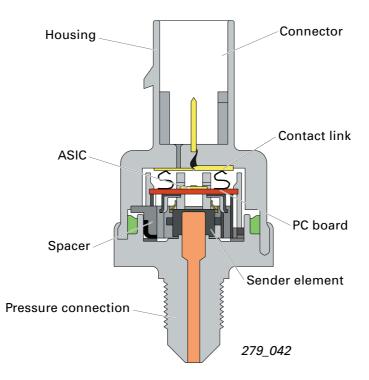
Engine sub-systems

Fuel pressure sender -G247

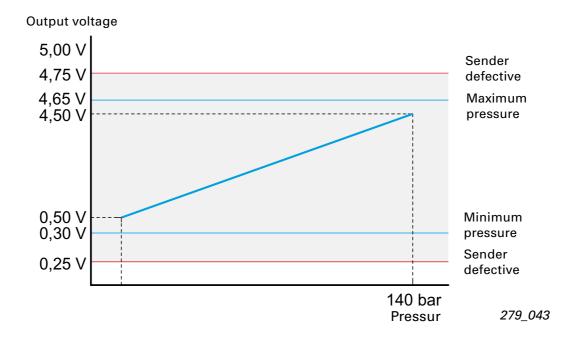
Within the overall system, the function of the fuel pressure sender is to measure the fuel pressure in the rail. The pressure applied is relayed to the engine control unit as a voltage quantity and used for fuel pressure control.

The evaluation electronics integrated into the sender are supplied with 5 V. With increasing pressure, the resistance drops and signal voltage rises.





The pressure sender characteristic curve illustrated shows signal output voltage [V] as a function of pressure [MPa].



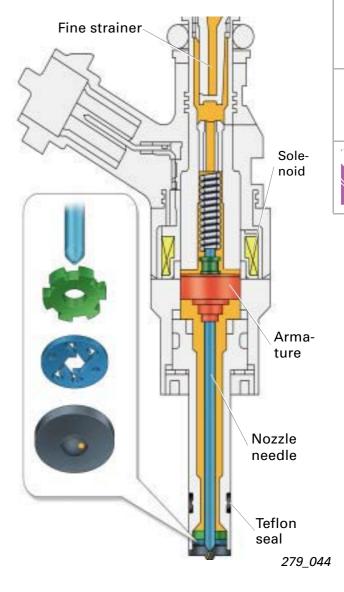
High-pressure injectors -N30, -N31, -N32, -N33

The high-pressure injector acts as an interface between the rail and the combustion chamber.

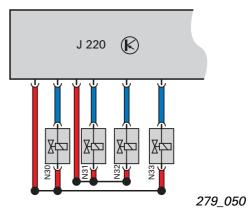
The function of the high-pressure injector is to meter the fuel and, by way of atomisation, to create a specific fuel/air mixture in a defined combustion chamber area (stratified charge or homogeneous operation).

On account of the difference between rail and combustion chamber pressure, injector actuation causes the fuel to be forced directly into the combustion chamber.

The Teflon seal always has to be replaced after removing the injector (refer to Workshop Manual).



Two booster capacitors integrated into the engine control unit generate the necessary actuation voltage of 50 - 90 V required to ensure a much shorter injection period than with intake-manifold injection.



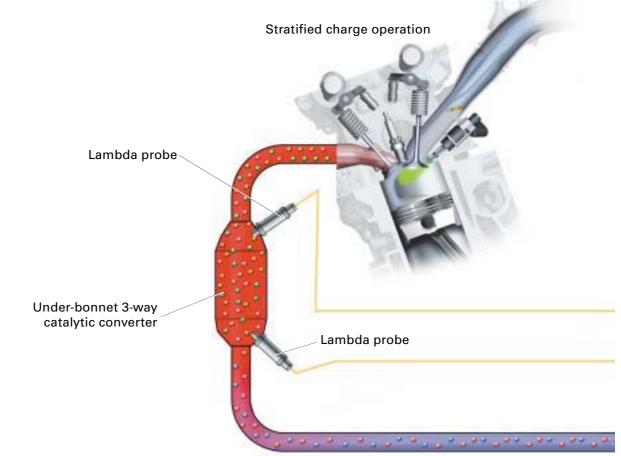
Engine sub-systems

Exhaust system

The ever increasing demands on exhaust systems as a result of reduced emission limits require an innovative concept specifically adapted to the FSI process.

2.0 | FSI engine

This engine features an under-bonnet threeway primary catalytic converter with an upstream and downstream probe for catalytic converter monitoring.



Exhaust-gas temperature sender -G235

The sender is located directly upstream of the $\ensuremath{\mathsf{NO}_x}$ storage catalytic converter.

It transmits the exhaust-gas temperature to the engine control unit for calculation of the temperature in the NO_x storage catalytic converter.

The engine-management system requires this information

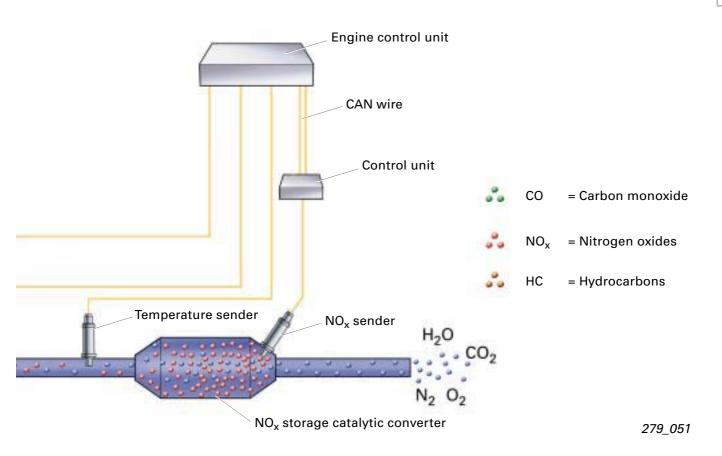
- For switching to stratified charge operation, as nitrogen oxides can only be stored in the NO_x catalytic converter at temperatures between 250 and 500 °C
- To remove sulphur deposits from the NO_x storage catalytic converter.
 This is only possible at catalytic converter temperatures above 650 °C with a rich mixture and is achieved by way of switching to homogeneous operation and ignition retard.



Exhaust gas treatment system

With a lean mixture composition, the conventional three-way catalytic converter exhibits a high conversion rate for CO and HC on account of the high residual oxygen content of the exhaust gas. The NO_x conversion rate drops however if CO and HC concentrations are too low.

Use is made of the NO_x storage catalytic converter to reduce the increased NO_x component in lean operation (stratified charge operation).



NO_x storage catalytic converter

The design of this converter corresponds to that of the three-way catalytic converter. The wash coat is however additionally provided with barium oxide to permit buffer storage of nitrogen oxides at temperatures between 250 and 500 °C through nitrate formation.

In addition to the desired nitrate formation, the sulphur contained in the fuel is always stored as well. The storage capacity is however limited. The engine control unit is informed of saturation by the NO_x sender and the enginemanagement system then takes appropriate action to regenerate the NO_x storage catalytic converter.

Engine sub-systems

Regeneration phases

These are regulated by the engine control unit and are designed to extract the nitrogen oxides and sulphur. In this process, nitrogen oxides are converted into non-toxic nitrogen and sulphur into sulphur dioxide.



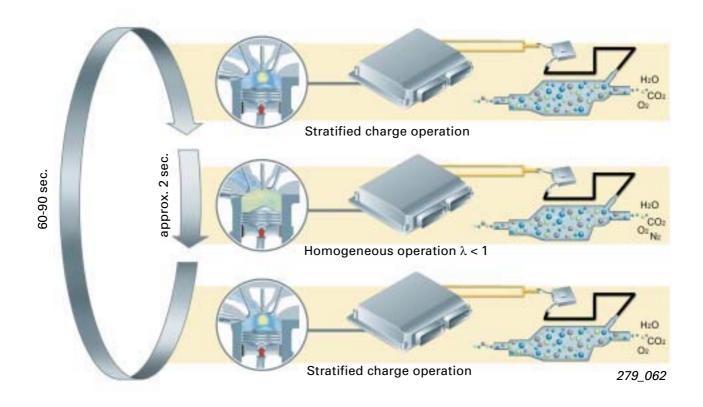
Nitrogen oxide regeneration

This takes place as soon as the concentration in the NO_x storage catalytic converter exceeds the level specified in the engine control unit.

The engine control unit effects switching from stratified charge to homogeneous operation.

This causes the temperature of the NO_x storage catalytic converter to increase. The nitrates formed thus become unstable and decompose under reducing ambient conditions.

The nitrogen oxides are converted into harmless nitrogen. The storage catalytic converter is thus emptied and the cycle recommences.

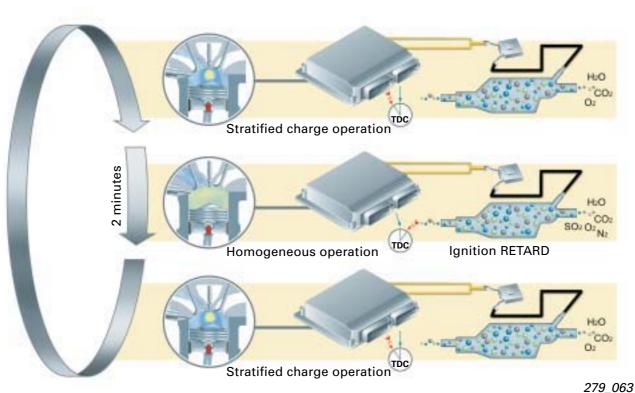


Sulphur regeneration

This takes place in separate phases, as the sulphates formed are more chemically stable and therefore do not decompose in the course of nitrogen oxide regeneration. The sulphur also occupies storage space, with the result that the storage catalytic converter becomes saturated at ever shorter intervals. As soon as the specified value is exceeded, the engine-management system reacts by implementing the following action:

- Switching from stratified charge to homogeneous operation for approx. two minutes and
- Ignition retard

This increases the catalytic converter operating temperature to above 650 °C, which causes the sulphur stored to react to form sulphur dioxide SO_2 .



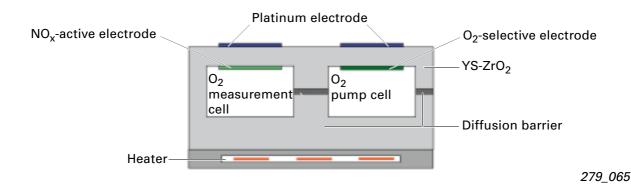
With low-sulphur fuels, the desulphurisation interval is correspondingly longer, whereas high-sulphur fuels necessitate more frequent regeneration phases. Driving at high engine speed under heavy load automatically leads to desulphurisation.

Engine sub-systems

NO_x sender -G295

The sender is located directly downstream of the NO_x storage catalytic converter. The NO_x sender operates in a manner similar to the wide-band Lambda probe.

In the first pump cell, the oxygen content is adapted to a constant, roughly stoichiometric value (14.7 kg of air : 1 kg of fuel) and the Lambda value picked off via the pump flow. The gas flow is then routed via a diffusion barrier into the O_2 measurement cell, where reducing electrodes separate the nitrogen oxides into oxygen (O_2) and nitrogen (N_2). The NO_x concentration is determined by way of the pump oxygen flow.



Control unit for NO_x sender -J583

This is located on the underside of the vehicle next to the NO_x sender. It conditions the sender signals and transmits the information to the engine control unit by way of the drive CAN bus.

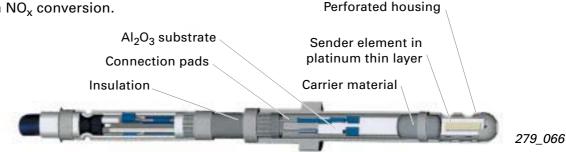
The rapid data transfer enables the engine control unit to establish nitrogen-oxide saturation more effectively and to initiate regeneration of the storage catalytic converter.

Exhaust-gas temperature sender -G235

This is located directly upstream of the NO_x storage catalytic converter.

The exhaust-gas temperature sender permits monitoring and control of the operating range of the NO_x storage catalytic converter with respect to temperature to ensure optimum NO_x conversion.

In addition, the exhaust-gas temperature sender is used for thermal diagnosis of the primary catalytic converter, to support the exhaust-gas temperature model and to protect components in the exhaust system.





Exhaust-gas recirculation

The engine features external exhaust-gas recirculation. The exhaust gas is extracted by way of a connecting pipe at the primary catalytic converter. The volume of exhaust gas calculated precisely by the engine control unit is fed in via the exhaust throttle valve, which is driven by an electric motor. The position of the exhaust throttle valve is monitored by a potentiometer. It permits calculation of the exhaust gas volume and is used for self-diagnosis.

The exhaust gas returned to the combustion chamber is used to lower the peak combustion temperature and thus reduce nitrogen oxide formation.

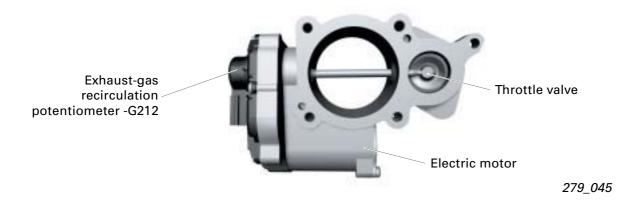




The exhaust-gas recirculation valve -N18 takes the form of a module and comprises the following components:

Exhaust-gas recirculation takes place in stratified charge/homogeneous operation at up to approx. 4000 rpm with medium load. There is no EGR at idle.

- Throttle valve
- Electric motor with exhaust-gas recirculation potentiometer -G212



Adaption by way of "basic setting" function must always be performed after replacing exhaust-gas recirculation valve and/or engine control unit.

Engine

Block diagram

Motronic ME7.1.1

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- Clutch pedal switch Brake light switch Map-controlled engine cooling thermostat F36 F47 F265
- Coolant temperature sender Fuel pump i Engline speed sender Lambda probe
- Intake-air temperature sender Knock sensor 1
- Coolant temperature sender Knock sensor 2
- Air-mass meter Intake-manifold pressure sender Accelerator position sender Coolant temperature sender radiator outlet
- G130 Landda probe after catalyst G130 Lamdda probe after catalyst G185 Throttle valve drive angle sender 1 G187 Throttle valve drive angle sender 1 G188 Throttle valve drive angle sender 2 G188 Throttle valve drive angle sender 2 G281 Throttle valve drive angle sender 2 G285 Exhaust-gas reinclation G237 Fuel pressure sender G237 Fuel pressure sender G236 NO_x sender G236 NO_x sender G336 Intake-manifold flap potentiometer

- B Exhaust-gas recirculation valve
 Injector, cylinder 1
 Injector, cylinder 2
 Injector, cylinder 3
 Injector, cylinder 4
 Injector, cylinder 4
 Injector, cylinder 4
 Activated charcoal filter solenoid valve N18 N30 N32 N33 N70 N80

TD signal (Multitronic only)

- N127 Ignition coil 2 with output stage N205 Canshaft adjustment valve N205 Intake manifold flap changeover valve N290 Teul metering valve N291 Ignition coil 3 with output stage N291 Ignition coil 4 with output stage P Shark plug connector C Shark plug connector V274 Fan for control unit

- = Output signal
- - = Earth

 - = CAN bus
- = Bidirectional
- Additional signals (1) K-wire
 - J17 Fuel pump relay
 J271 Motronic current supply relay
 J338 Throttle valve control part
 J583 Control unit for NO_x sender

CAN High/drive

CAN Low/drive

N M

Alternator test signal Radiator fan PWM

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- = Input signal

- = Positive supply

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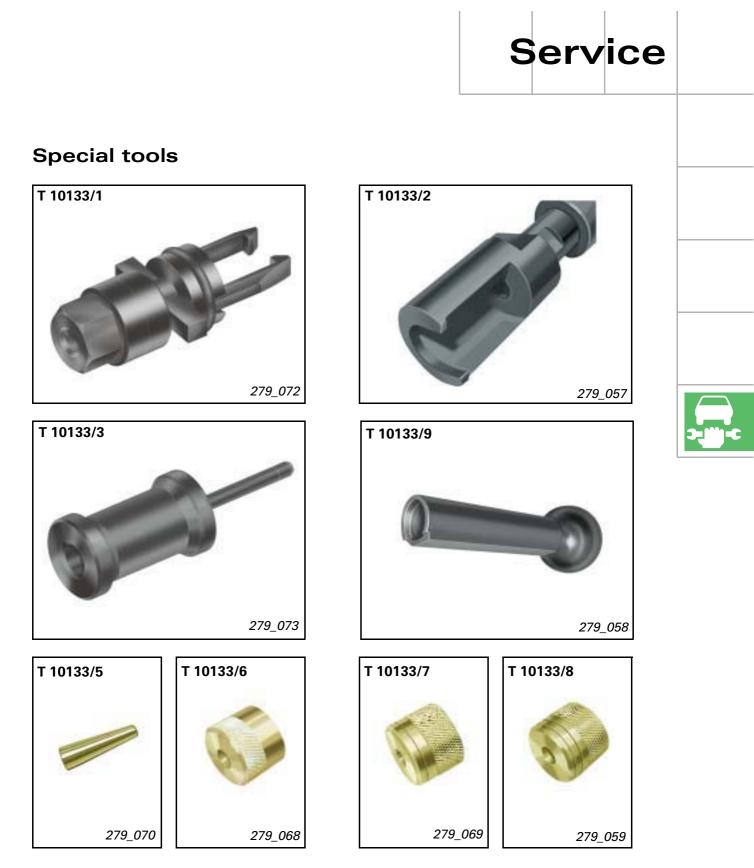
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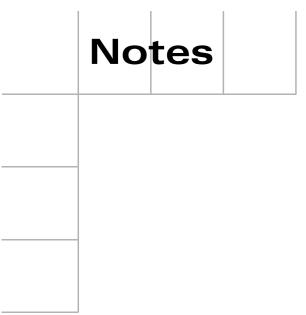
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